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The cost of satisfying structural design requirements on progressive collapse resistance

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*Final Conference
COST Action TU0601 'Robustness of Structures'
Prague, Czech Republic
30-31 May 2011*

Local / global requirements in design codes

- Contemporary design codes (e.g. Eurocodes) ensure structural safety through calibrated explicit requirements at the component / element / connection level
(LOCAL REQUIREMENTS)
- Structural system performance not accounted for explicitly (no explicit **GLOBAL REQUIREMENTS** specified)
- Global requirements:
 - system resistance requirements *(collapse resistance)*
 - robustness requirements *(progressive collapse resistance)*
- The incorporation of explicit global requirements in the design process will typically increase the cost of the structural system designed:
need for additional material

The cost of satisfying global requirements

- It is believed that, in several design cases, the satisfaction of global requirements (on top of local ones) will increase the cost of the structural system only *marginally*
- This additional cost actually depends on:
 - 'how much' system resistance and robustness we require
 - effectiveness of utilized tools and measures to satisfy new requirements
- Investigation needed on the additional cost induced by global requirements
- This investigation is performed in the framework of **structural design optimization of elastoplastic steel frames**

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Application

- Structural design optimization of elastoplastic steel frames
- Integrated design optimization approach accounting for *local and global* structural performance requirements
- Aims:
 - Progressive collapse resistance assessment of elastoplastic steel frames
 - Investigation of cost due to additional system performance requirements
 - Gain insight on the way the optimization procedure manages to meet system performance / robustness requirements

Thus, actual aim is to:
'discover' how to meet robustness requirements with minimum cost (learn from optimization results)
- Input to:
 - Activity 8: Robustness assessment of selected classes/types of structures/materials.*

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Measuring progressive collapse resistance

Intact structure

Limit load factor
 α_c

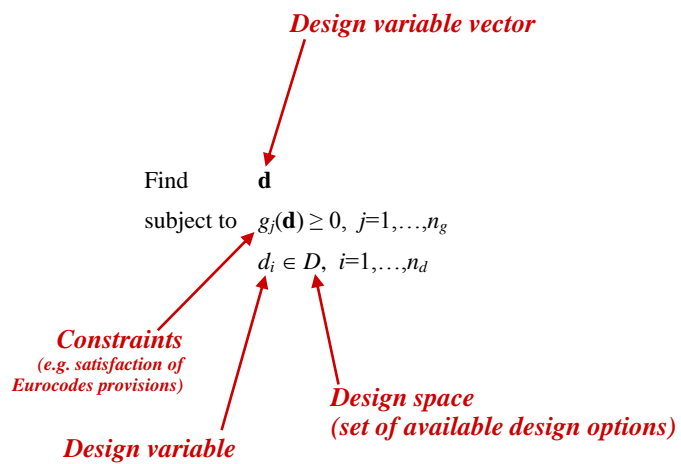
'Damaged' structure
(notional column removal)

Limit load factor
 α_{cd}

Progressive collapse resistance index: $\rho = \frac{\alpha_{cd}}{\alpha_c}$

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Code-based design



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Cost-oriented design optimization

Cost

$$\begin{aligned} &\text{minimize} && C(\mathbf{d}) \\ &\text{subject to} && g_j(\mathbf{d}) \geq 0, \quad j=1, \dots, n_g \\ & && d_i \in D, \quad i=1, \dots, n_d \end{aligned}$$

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Cost-oriented design optimization with additional system performance requirements

$$\begin{aligned} &\text{minimize} && C(\mathbf{d}) \\ &\text{subject to} && g_j(\mathbf{d}) \geq 0, \quad j=1, \dots, n_g \\ & && \alpha_c(\mathbf{d}) \geq \alpha_{c,\min} \\ & && \rho(\mathbf{d}) \geq \rho_{\min} \\ & && d_i \in D, \quad i=1, \dots, n_d \end{aligned}$$

Collapse load factor of undamaged structure

(design \mathbf{d} satisfies EC3 requirements)

Collapse resistance requirement

Progressive collapse resistance requirement

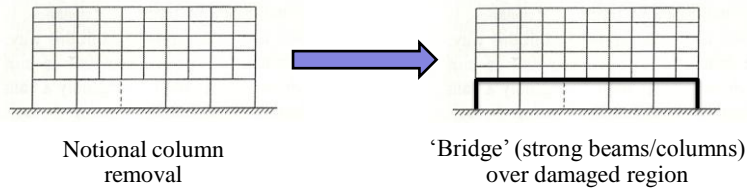
min allowable values

Progressive collapse resistance index $\rho = \frac{\alpha_{cd}}{\alpha_{c,\min}}$

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The alternate path method with notional column removal

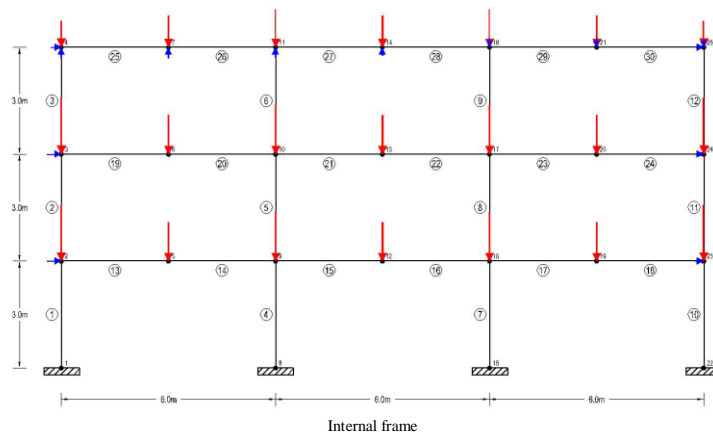
- **Aims:**
 - redistribution of loads on damaged structure to remaining undamaged members
 - loads safely transferred to ground through alternate load paths
- Obvious implementation of alternate path method: **'bridge' formation over damaged region**



- **Disadvantages of 'bridge'-philosophy:**
 - local strengthening only (*column removal at storey higher than the 'bridge'?*)
 - is it the most economical way of strengthening?
- The design optimization approach of the present work ensures the satisfaction of progressive collapse resistance requirements using the alternate path method with **minimum cost**

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Test example 1: 3-storey frame



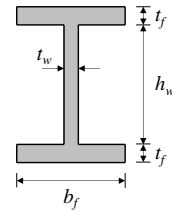
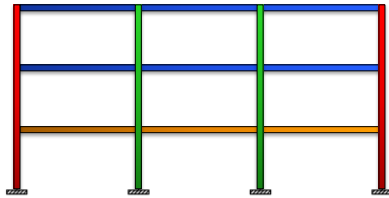
- Subjected to dead, live and wind load
- For limit load elastoplastic analysis
 - Constant dead and live loads
 - Variable wind loads

Test example 1: 3-storey frame

- Modeling

- 4 member categories (16 design variables)
- Each member category: 4 design variables

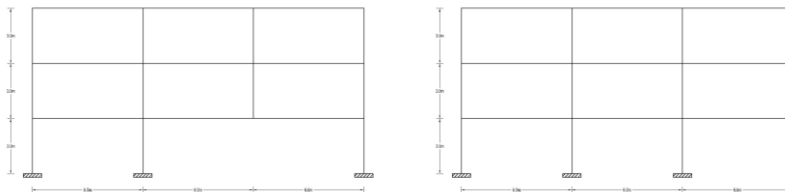
- 1st Cat. – Corner columns
- 2nd Cat. – Internal columns
- 3rd Cat. – Beams of storey 1
- 4th Cat. – Beams of storeys 2-3



Test example 1: 3-storey frame

- Damage scenarios analyzed

- Removal of an internal column
- Removal of a corner column



- Optimization analysis

- Aim: minimize total material volume of intact structure
- Results obtained for $\alpha_{c,min}=30$ and various values of ρ_{min} imposed

Test example 1: 3-storey frame

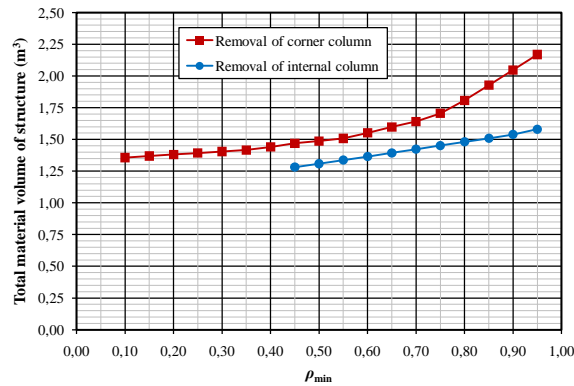
- Total material volume of structure

- **Removal of internal column**

$\rho_{\min}=0.45$ ($\alpha_c=30 \rightarrow \alpha_c=15$)
 For demand $\rho_{\min}=0.95 \rightarrow 23\%$ increase
 in total material volume

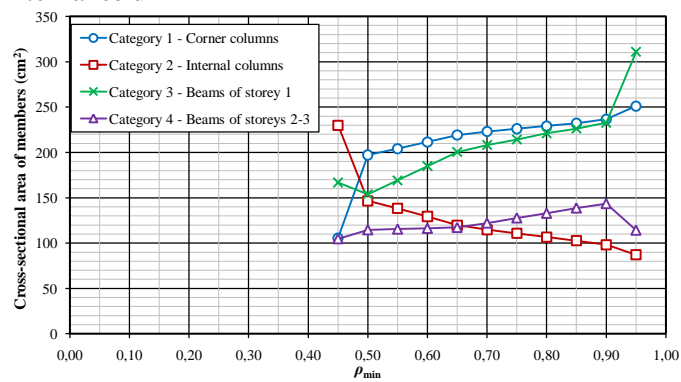
- **Removal of corner column**

$\rho_{\min}=0.10$ ($\alpha_c=30 \rightarrow \alpha_c=3$)
 For demand $\rho_{\min}=0.95 \rightarrow 60\%$ increase
 in total material volume



Test example 1: 3-storey frame

- Removal of internal column**

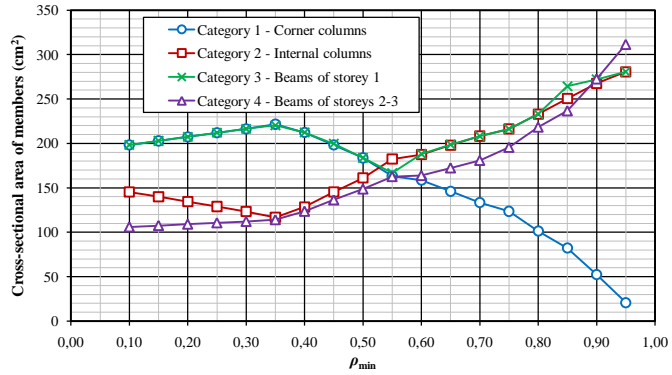
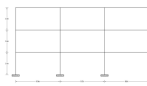


- Behavior**

- Gradual strengthening of corner columns and beams of storey 1 – **'bridge'**
- Mild strengthening of beams of storeys 2-3
- Gradual decrease in the dimensions of the internal columns

Test example 1: 3-storey frame

- Removal of corner column



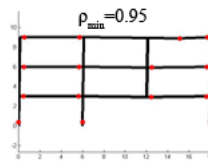
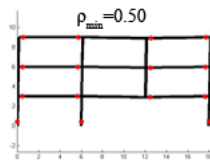
- Behavior

- Low resistance demands: Local approach with the formation of 'bridge'
- High resistance demands: Global approach with the strengthening of all members except for corner columns

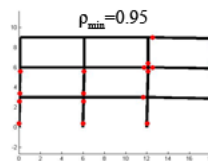
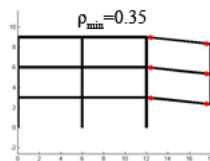
Test example 1: 3-storey frame

- Collapse mechanism of the damaged frame

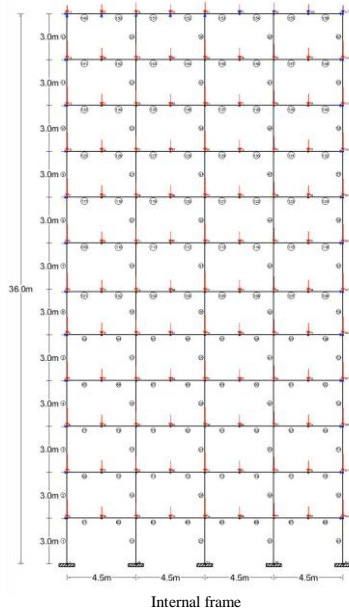
- Removal of internal column



- Removal of corner column



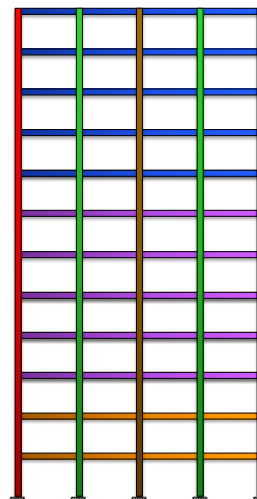
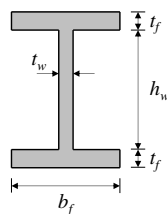
Test example 2: 12-storey frame



- Subjected to dead, live and wind load
- For limit load elastoplastic analysis
 - Constant dead and live loads
 - Variable wind loads

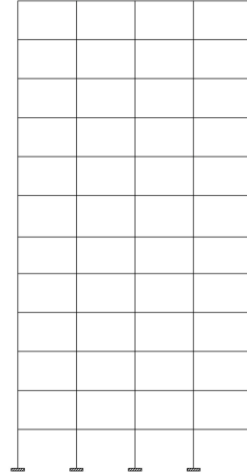
Test example 2: 12-storey frame

- Modeling
 - 6 member categories (24 design variables)
 - 1st Cat. – Corner columns
 - 2nd Cat. – Internal columns
 - 3rd Cat. – Central columns
 - 4th Cat. – Beams of storeys 1-2
 - 5th Cat. – Beams of storeys 3-7
 - 6th Cat. – Beams of storeys 8-12
 - Each member category: 4 design variables



Test example 2: 12-storey frame

- Damage scenarios analyzed
 - Removal of a central column
 - Removal of a corner column
- Optimization analysis
 - Aim: minimize total material volume of intact structure
 - Results obtained for $\alpha_{c,min}=7$ and various values of ρ_{min} imposed



Test example 2: 12-storey frame

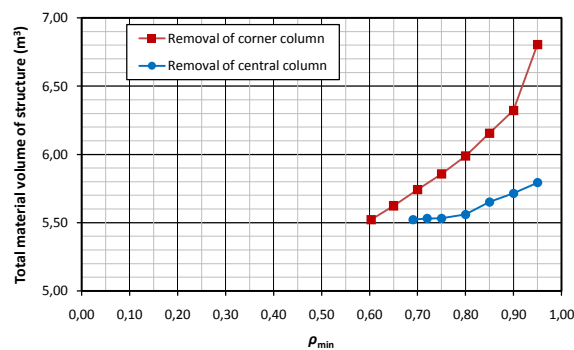
• Total material volume of structure

– Removal of central column

$\rho_{min}=0.69$ ($\alpha_c=7 \rightarrow \alpha_c=4.8$)
 For demand $\rho_{min}=0.95 \rightarrow 4.9\%$ increase
 in total material volume

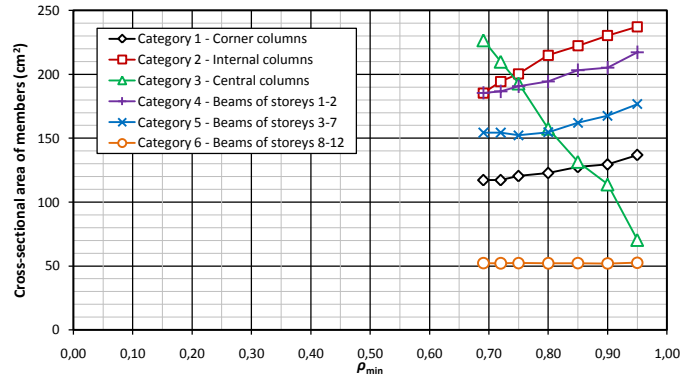
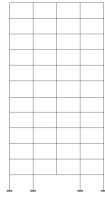
– Removal of corner column

$\rho_{min}=0.60$ ($\alpha_c=7 \rightarrow \alpha_c=4.2$)
 For demand $\rho_{min}=0.95 \rightarrow 23.2\%$ increase
 in total material volume



Test example 2: 12-storey frame

- Removal of central column

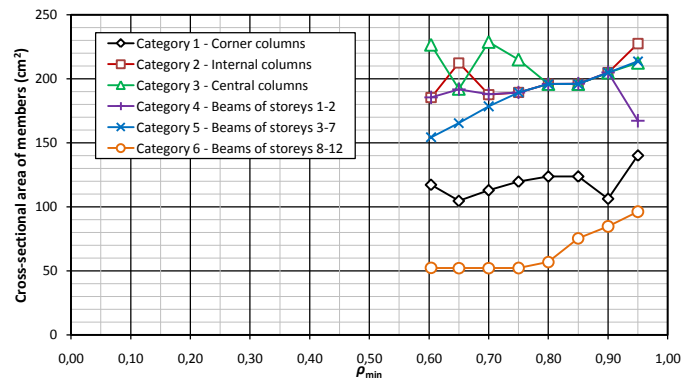
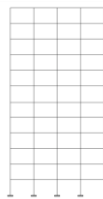


- Behavior

- Gradual strengthening of all elements (except central columns)
- Incline towards strong columns (mostly internal) – central columns with decreased participation
- Reduced participation of beams of higher storeys

Test example 2: 12-storey frame

- Removal of corner column



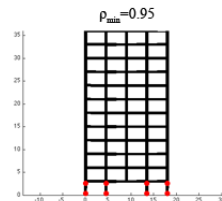
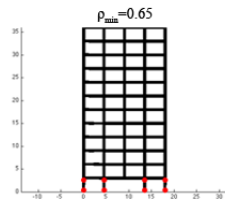
- Behavior

- Similar behavior as previously
- Gradual strengthening of all elements
- Incline towards strong columns – corner columns at lower levels
- Reduced participation of beams of higher storeys

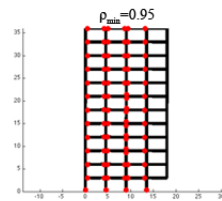
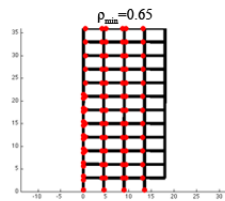
Test example 2: 12-storey frame

- Collapse mechanism of the damaged frame

- Removal of central column



- Removal of corner column



Conclusions

- It is not possible to know a-priori the *optimal* amount and allocation of additional material required, in order to satisfy progressive collapse resistance constraints
(depends on structural system, material/geometric properties, loads, demand on collapse resistance, etc.)
 - ➔ Every problem is a case of its own, which has to be optimized explicitly
 - ➔ Practically infeasible to fully substitute optimization by simple guidelines
 - ➔ Rather macroscopic conclusions obtainable, not detailed quantified rules
- The increase in material demand varies almost linearly for low and moderate progressive collapse resistance requirements.
For high progressive collapse resistance requirements this relation becomes non-linear causing higher demands in material.

Conclusions

- **Low-rise buildings** (e.g. 3-storey frame)

Internal column removed:

the optimizer tends to produce strong corner columns and strong beams at storey 1, forming this way a type of ‘**bridge**’ over the damaged region
(structural system activated locally)

Corner column removed:

for relatively high progressive collapse resistance requirements, the optimizer tends to yield strong internal columns and **strong beams at all storeys**, while corner columns contribute very little *(structural system activated globally)*

- **High-rise buildings** (e.g. 12-storey frame)

Central or corner column removed:

the optimizer tends to introduce strong columns and **strong beams at all storeys** except for the few highest storeys *(structural system activated globally)*

As the demand for progressive collapse resistance becomes higher, the optimizer invokes more and stronger beams over the height of the structure
(activation of the structure as a system against the damage effect)